

3D numerical simulation of the electric arc motion between bus-bar electrodes

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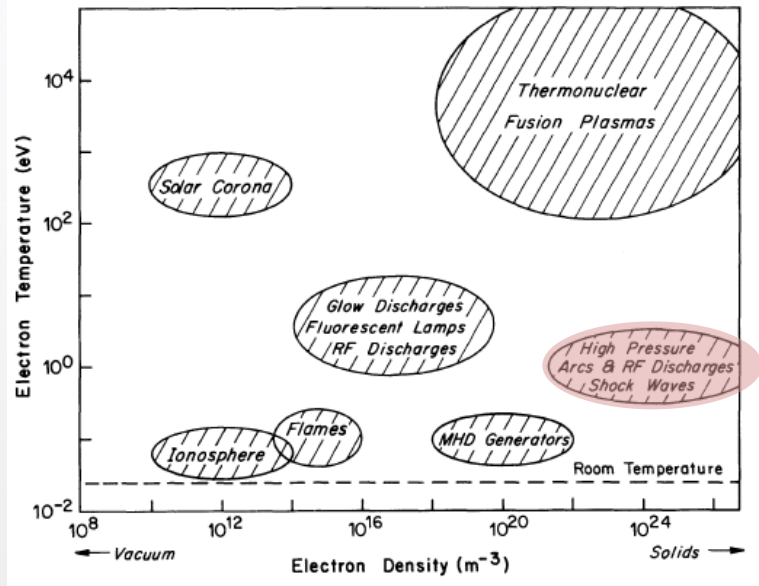
**COMSOL
CONFERENCE**
2017 ROTTERDAM

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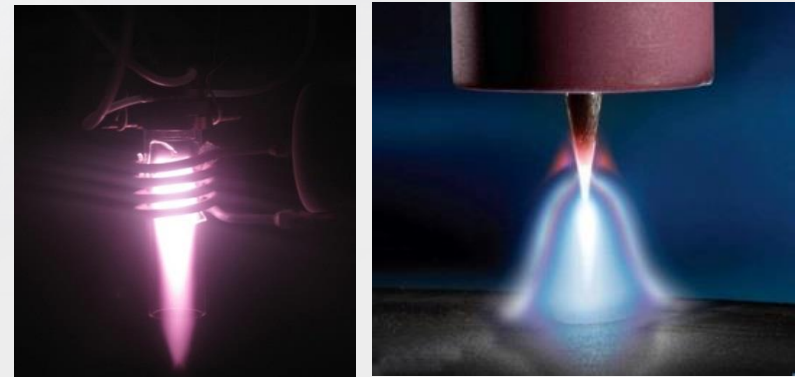


Thermal plasmas

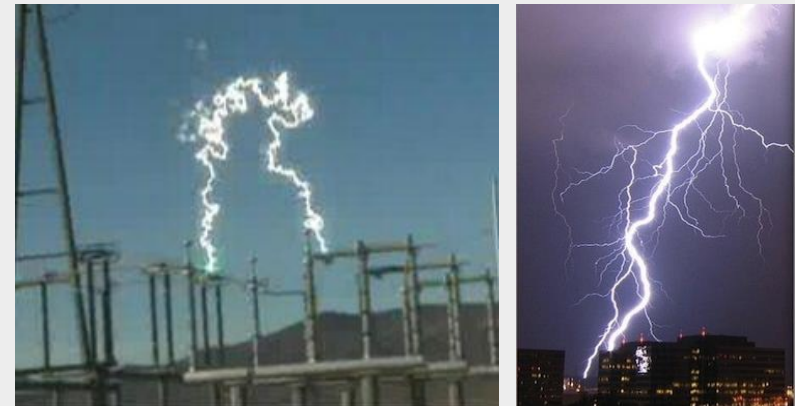
Plasmas classification [1]:



Thermal plasma applications:



Thermal plasma in nature:



Thermal plasmas characteristics:

$$n_e \sim 10^{21} - 10^{26} \text{ m}^{-3} \quad \text{and} \quad T_e \sim 10^4 \text{ K}$$

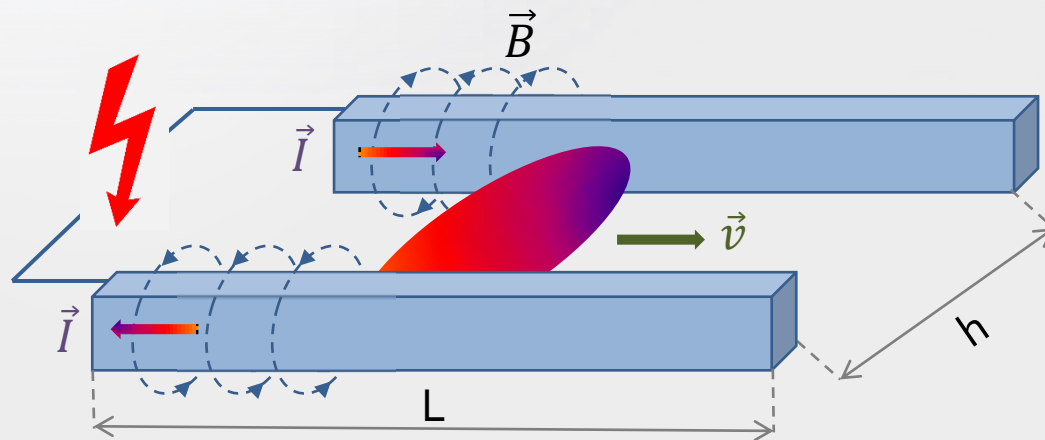
Local Thermodynamic Equilibrium (LTE)

Objective

Bus-bars electrodes construction, dimensions: $L \sim 100 - 200$ mm and $h \sim 10$ mm

Supplied with AC or DC currents in range $100 - 1000$ A

Working conditions: $0.1 - 1$ atm



In case of fault the **electric arc takes place and propagates along the electrodes.**

Goal: to investigate arc propagation using numerical simulation

Mathematical description

Arc column description and electrodes:

The system of MHD equations in the LTE approximation is solved for **arc bulk plasma**:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \mathbf{u} = 0,$$

$$\frac{\partial \rho \mathbf{u}}{\partial t} + \nabla \cdot \rho \mathbf{u} \otimes \mathbf{u} = -\nabla p + \nabla \cdot \eta (\nabla \mathbf{u} + (\nabla \mathbf{u})^T) - \frac{2}{3} \nabla (\eta \nabla \cdot \mathbf{u}) + \mathbf{j} \times \mathbf{B},$$

$$\rho c_p \left(\frac{\partial T}{\partial t} + \mathbf{u} \cdot \nabla T \right) + \nabla \cdot \mathbf{q} = -\mathbf{j} \cdot \nabla \varphi - Q_{rad}, \quad \mathbf{q} = -\lambda \nabla T - \frac{5 k T}{2 e} \mathbf{j},$$

$$\nabla \cdot \mathbf{j} = 0, \quad \mathbf{j} = -\sigma \nabla \varphi,$$

$$\nabla \times \frac{1}{\mu_0} \mathbf{B} = \mathbf{j}, \quad \mathbf{B} = \nabla \times \mathbf{A}.$$

In the electrodes:

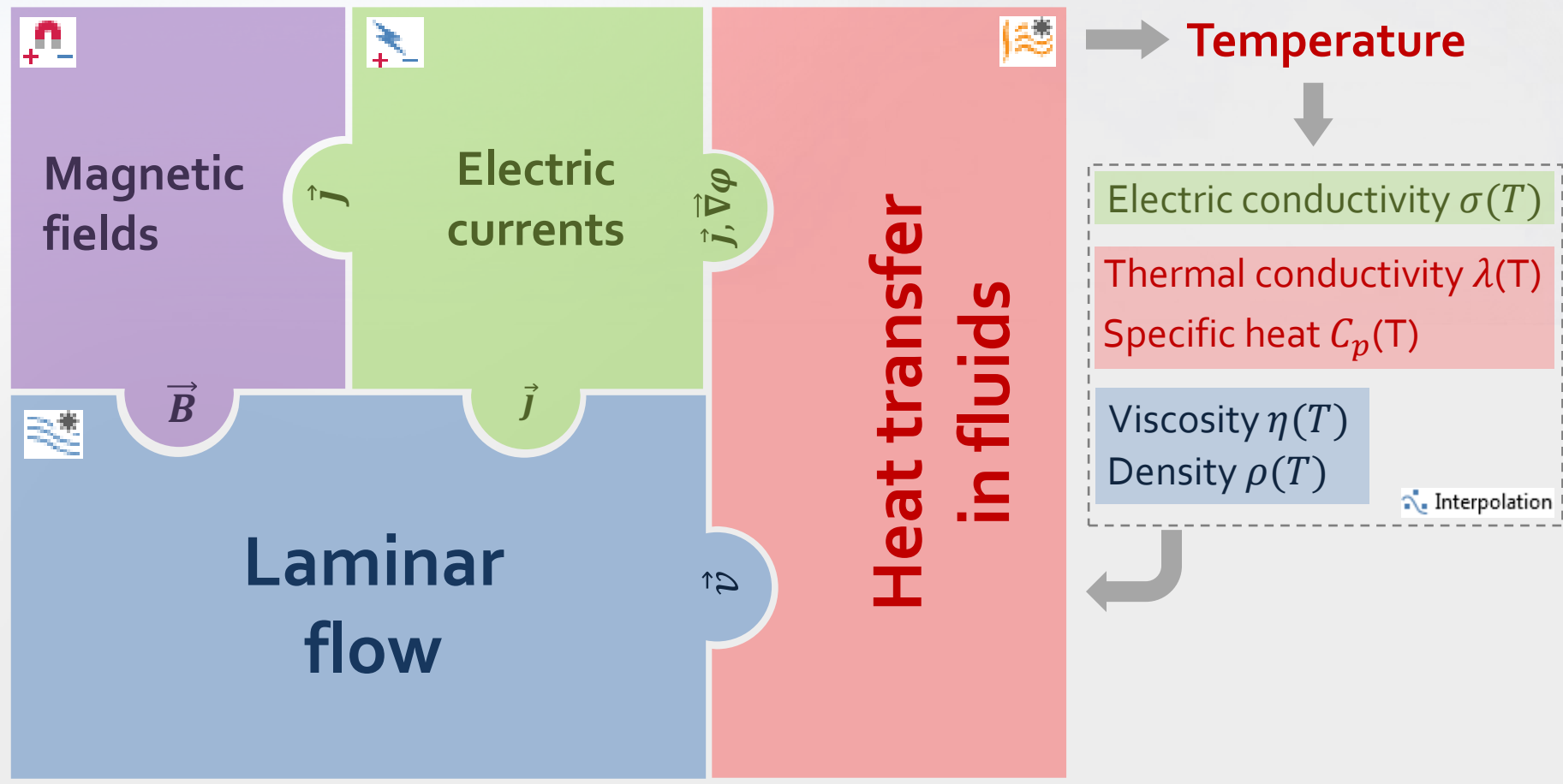
$$\rho_s c_p \nabla \frac{\partial T_s}{\partial t} \cdot (\lambda_s \nabla T_s) + \sigma_s (\nabla \varphi)^2 = 0,$$

$$\nabla \cdot (\sigma_s \nabla \varphi) = 0.$$

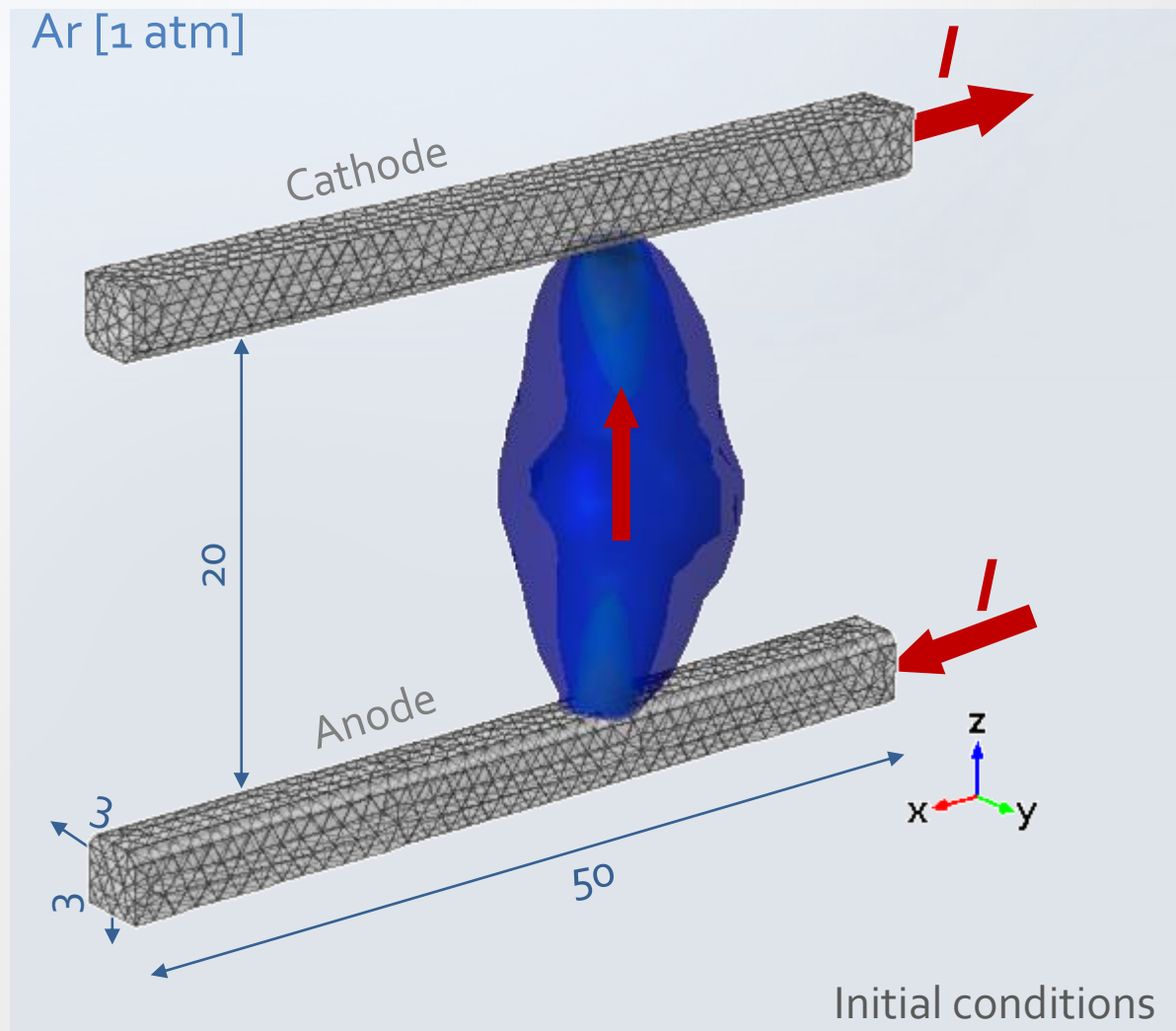
$$\nabla \times \frac{1}{\mu_0} \mathbf{B} = \mathbf{j}, \quad \mathbf{B} = \nabla \times \mathbf{A}.$$

The system is solved with respect to variables: $\mathbf{u}, p, T, \varphi, \mathbf{A}$ in the arc plasma
and
 φ, T_s, \mathbf{A} in the electrodes.

Arc model in COMSOL



Calculation conditions



Electrodes:
Plane electrodes
made of copper

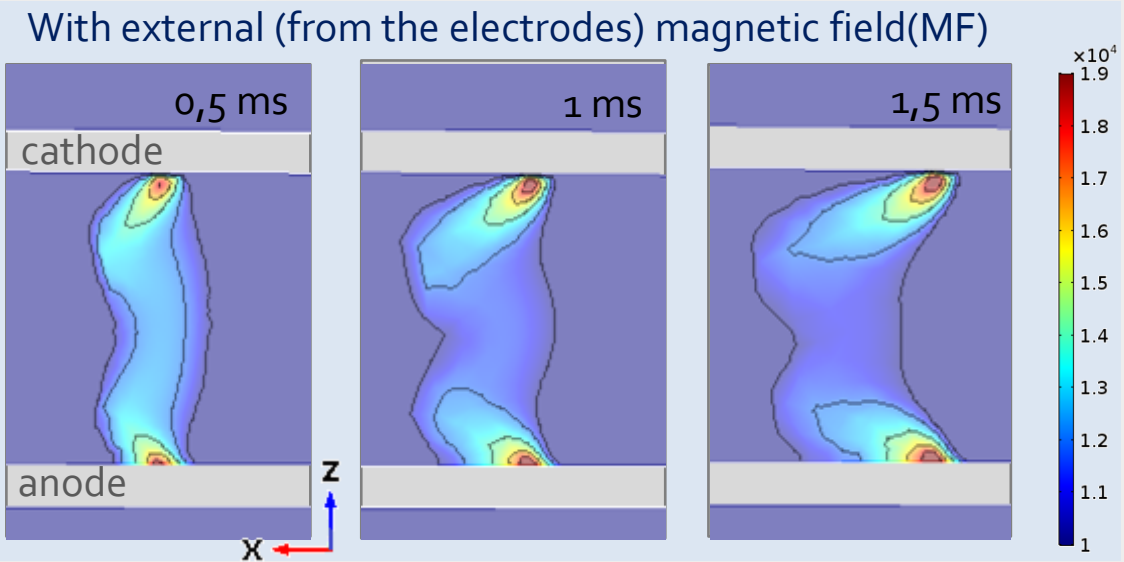
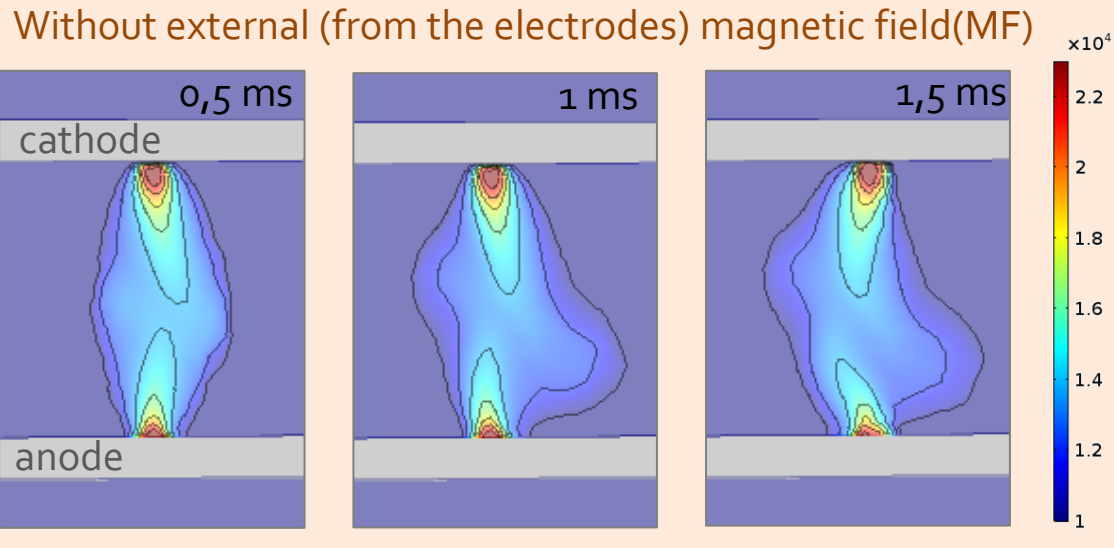
Power:
Direct current
I = 200 A

Conditions:
Atmospheric pressure
Gas: argon

Initial conditions:
Stationary arc with,
fixed spots positions.

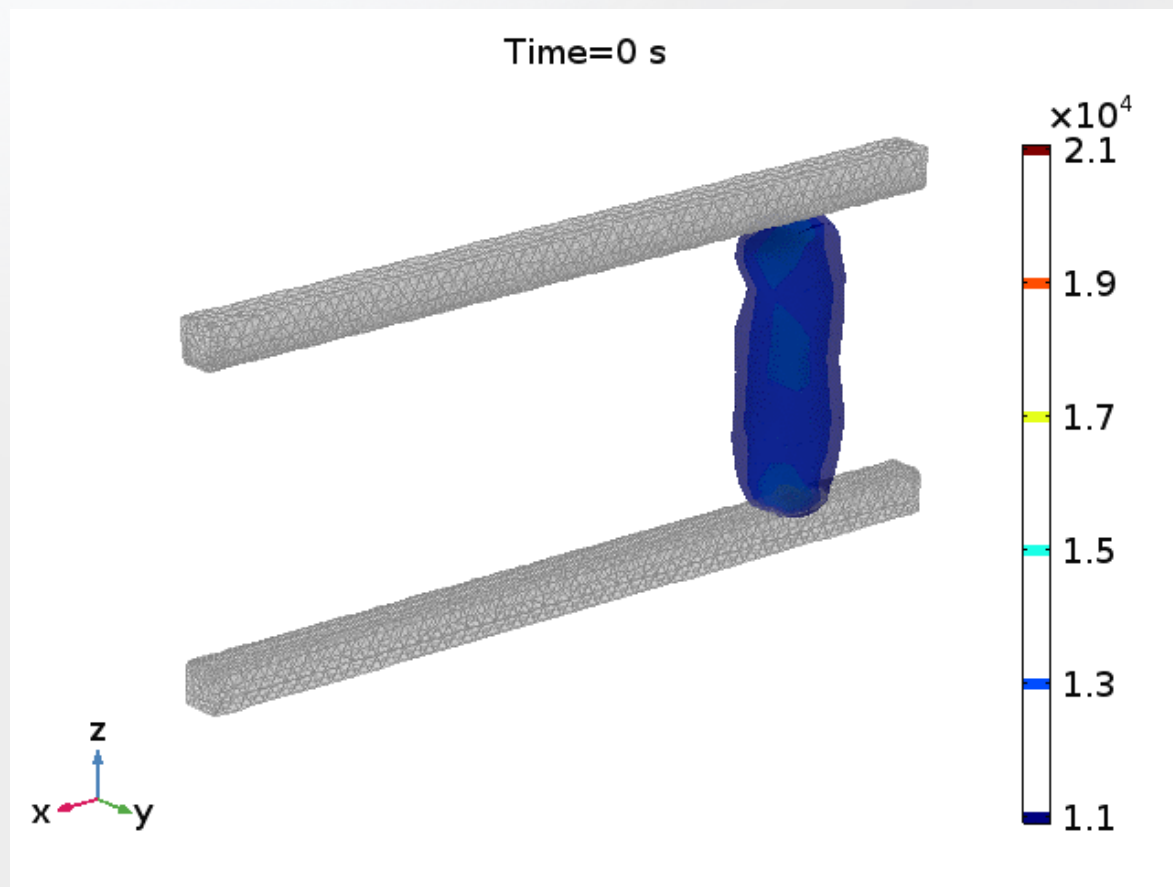
Impact of the magnetic field

Temperature (in K) distributions

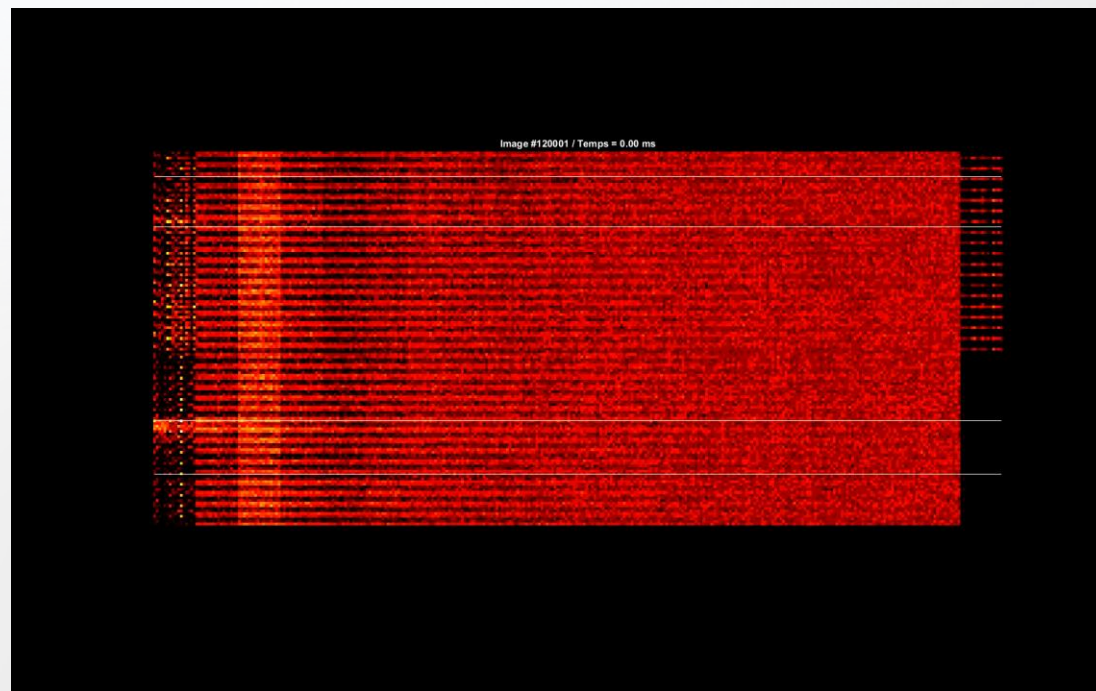


Arc displacement

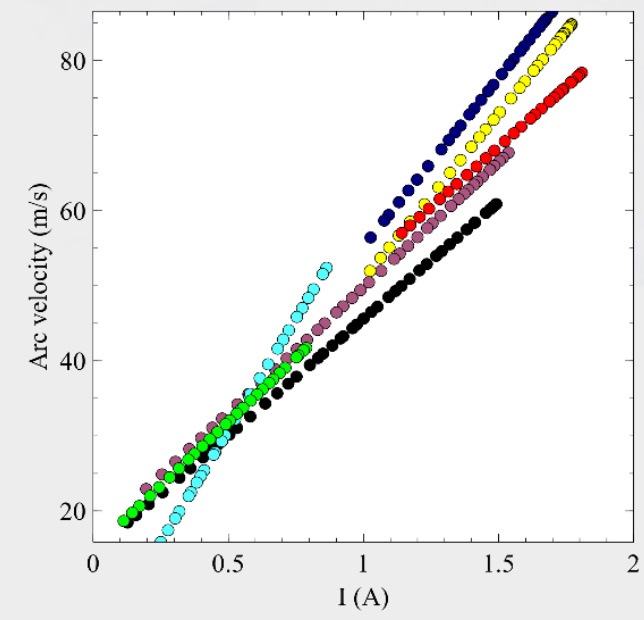
Arc temperature (in K) evolution with the time



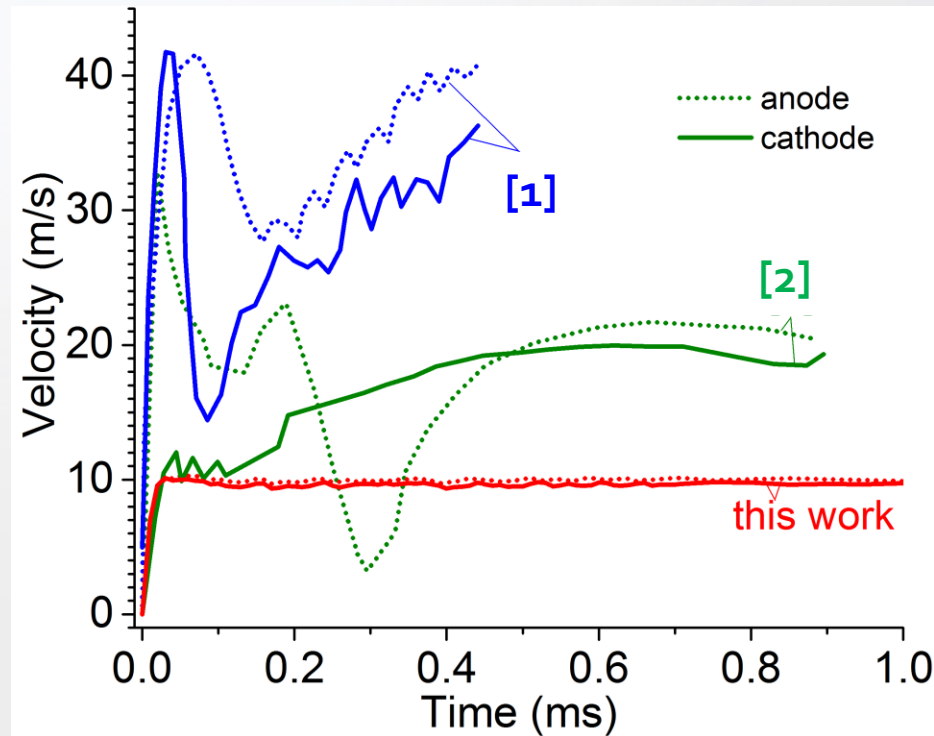
Experiment



$I = 1.5$ kA peak, $h = 20$ mm, 60 000 fr/s



Arc displacement velocity



[1] M.Lisnyak, M. Chnani, A. Gautier, J-M. Bauchire, "Behavior of a short electric arc between plane electrodes: numerical and experimental study", contributions to ICPIG congress, July 2017.

[2] B. Swierczynski, J. J. Gonzalez, P. Teulet, P. Freton, and A. Gleizes, "Advances in low-voltage circuit breaker modelling," 2004.

Numerical aspects

■ Stabilization

- Laminar flow 
 - Heat transfer in fluids 
- 
- Streamline diffusion
Crosswind diffusion

■ Discretization:

- Linear or quadratic basic functions.

■ Solver :

- Segregated ($\varphi, \mathbf{A}, \mathbf{u}, p, T$) \rightarrow Direct (MUMPS) and Iterative (GMERS).

■ Convergence criteria:

- Relative tolerance is 0.01.

■ Mesh:

- Number of DOF 10^6 , refined near the electrodes with $\Delta x_{\max} = 0.6$ mm.

■ Calculation time:

- 7 days with 8 cores, Xeon 3.2 GHz, 32 Gb.

Summary

- COMSOL Multiphysics® allows to perform 3D time-dependent model of the electric arc.
- The good numerical stability for highly nonlinear problems is achieved.
- The calculation time is reasonable, that makes the model interesting for engineering applications.
- The physical aspects of the model corresponds to the experimental observations.

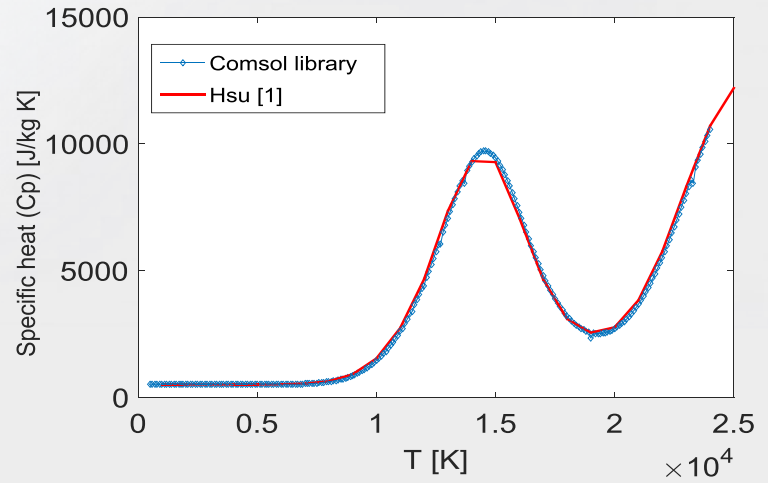
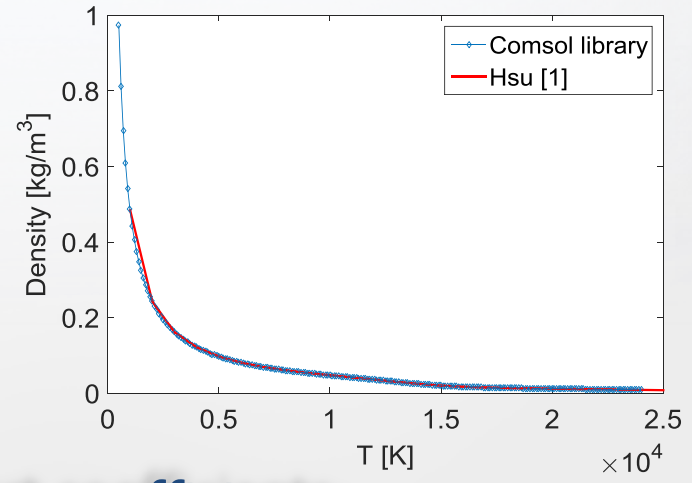
For more details I would like to invite you to
the **poster 84**.

Thank you!

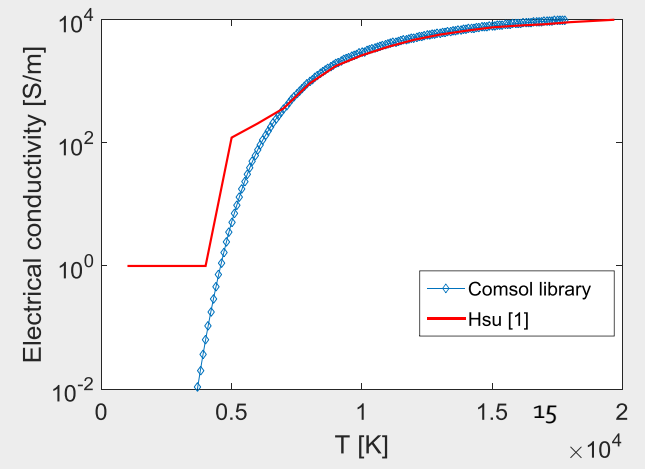
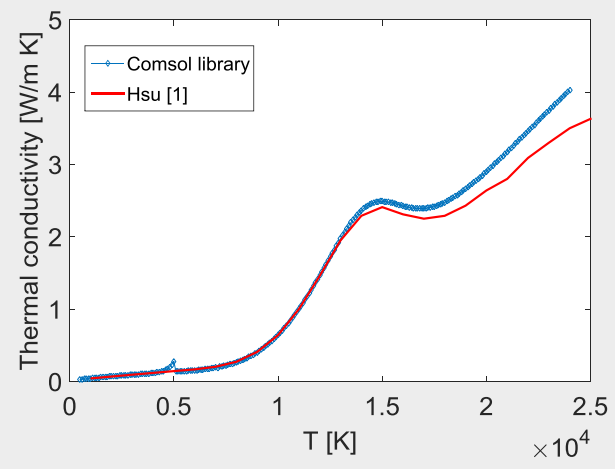
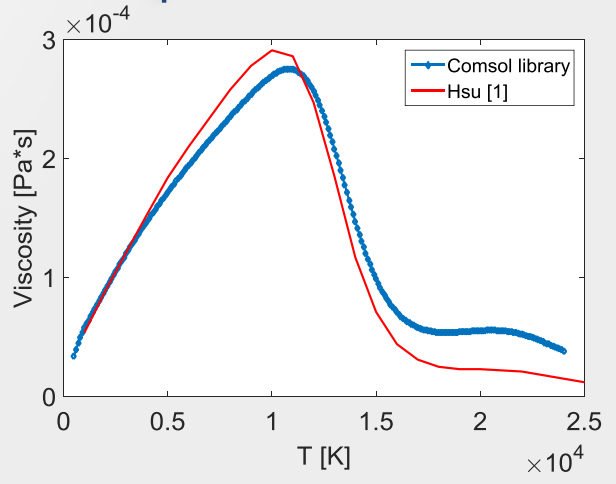
Plasma properties

Thermodynamic properties:

Argon 1 atm



Transport coefficients:



[1] K. C. Hsu, K. Etemadi, and E. Pfender, "Study of the free-burning high-intensity argon arc," *J. Appl. Phys.*, 1983.

Convergence control

Mass conservation

Integration over external surface of the model: $\oint (\rho \vec{v} \cdot \vec{dS}) \cong 0$

- 2 D case
$$\oint (\rho \vec{v} \cdot \vec{dS}) = 2\pi\rho \int_0^R v_z r dr + \rho R \int_0^h v_r dh = 0$$
- 3 D case
$$\oint (\rho \vec{v} \cdot \vec{dS}) = \oint \rho (v_x n_x + v_y n_y + v_z n_z) dS = 0$$

Where n_x, n_y, n_z are normal vectors (directed externally to the surface),
R – model radius, h – model height

Current conservation

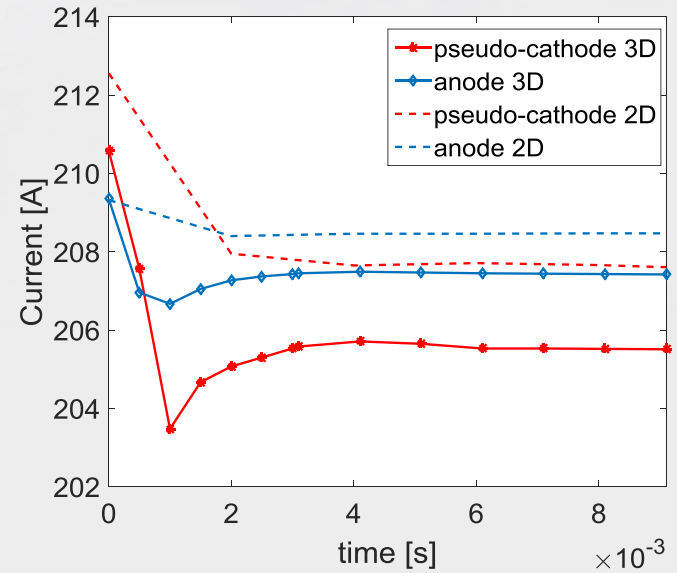
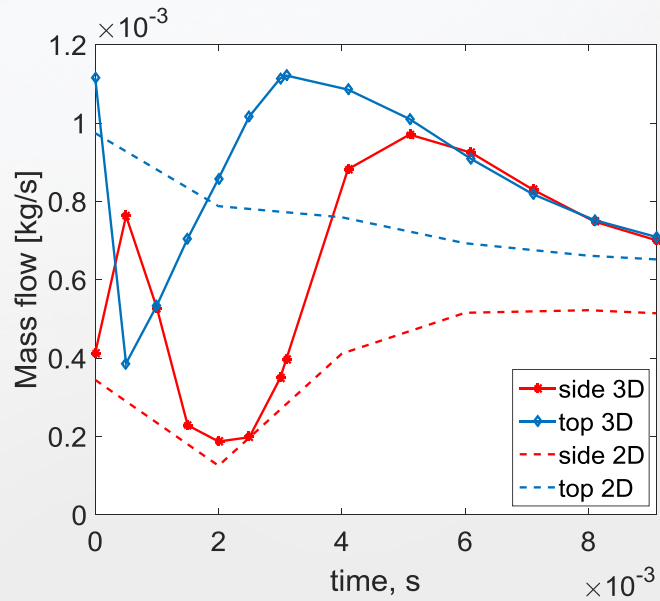
$$\oint (\vec{j} \cdot \vec{dS})_{cathode} = \oint (\vec{j} \cdot \vec{dS})_{anode}$$



In COMSOL MF

Results → Derived values →
Surface integration

Fluxes calculations



Arc – electrodes interaction

Plasma near the electrodes **is not in equilibrium**.

Goal: To include plasma-electrodes interaction without implementing non-equilibrium plasma description.

Plasma – anode interaction:

attachment is constricted (spot mode), $R_{as} = 0.8 \text{ mm}$.
anode heating is calculated according to:

$$q_a = \left(\frac{5}{2} kT_{\delta_{pl}} + A_f \right) \frac{j}{e}$$

Plasma – cathode interaction:

spot mode on the cathode with the fixed radius [1, 2]: $R_{cs} = 1 \text{ mm}$.
temperature in the cathode spot is uniformly distributed [1]: $T_{av} = 3200 \text{ K}$.

✓ The current continuity is imposed between plasma and electrodes.

[1] W. L. Bade and J. M. Yos, Theoretical and Experimental Investigation of Arc Plasma-generation Technology, 1963.

[2] M. S. Benilov and A. Marotta, "A model of the cathode region of atmospheric pressure arcs," J. Phys. Appl. Phys., vol. 28, no. 9, p. 1869, Sep. 1995.